

# Design and Analysis of Rocker Arm by Finite Element Method using ANSYS

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**Abstract**— The rocker arm is a fundamental component for valve actuating mechanism of an Internal Combustion engine. Over the years, several tests and analysis, considering factors such as weight, cost, stresses etc., has been carried out for optimization of rocker arms. The failure of rocker arm is an important concern. This paper deals with modelling and analysis of stresses developed in a rocker arm. The required model was designed using the Solidworks 2013 and finite element analysis was carried out using ANSYS 16.0 software.

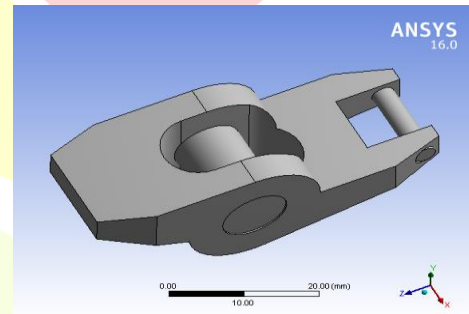


Fig. 2. CAD model of Rocker arm

**Index Terms**—ANSYS, Finite Element Analysis (FEA), Rocker arm, Solidworks.

## I. INTRODUCTION

The rocker arm, a component of an Internal Combustion engine, is a reciprocating two arm lever. One end of the arm is actuated by rotating lobe of camshaft while the other acts on the valve stem. The basic function of a rocker arm is opening and closing of the inlet and exhaust valve with respect to motion of cam and follower [1]. This allows fuel and air to be drawn into the combustion chamber during the intake stroke or exhaust gases to be expelled during the exhaust stroke [2].



Fig. 1. Rocker Arm Assembly<sup>[9]</sup>

It also provides a mean of multiplying the lift ratio. As a lever, its actual function is to change the direction of force and not effort multiplication. It conveys radial movement from the cam lobe into linear movement at the poppet valve to open it [3]. Different vehicles require different designs and specifications of rocker arms. The type of internal combustion engine also determines the types of rocker arms. The mechanical advantage of rocker arm is termed as 'Rocker ratio'. Rocker arms are used to control both the intake and exhaust valves, swapping high-ratio rocker arms onto an engine increases both the intake-air command and the exhaust-scavenging potential. Generally speaking, a bump in rocker-arm ratio results in a noticeable performance gain [4]. In moderate and low speed engine, 1:1 ratio is used while for high speed engines it is around 1:1.3

The rocker arm for exhaust valve is heavily loaded and requires more force for operation compared to inlet valve. But in practice, for ease of manufacturing, rocker arms for both inlet and exhaust are identical [5].

The various forces act on the arms during the operation. These forces can be mainly categorized into:

1. Gas pressure on valve, which comes into play when valve opens

2. Inertia force, which opposed the upward movement of the valve

3. Inertial Spring force, which hold the valve on its seat against the suction.

The Failure of rocker arm is an important concern as it is an important component of IC engine. Several failure analysis has been made till now. Stresses and vibrations during the engine operation results in deflection of rocker arms. It was observed that initiation and growth of the cracks was facilitated by a microstructure of low fatigue strength and multiple-origin fatigue was dominant failure mode [1].

Lee, Cho & Joo observed that the failure of the rocker arm shaft was caused by the bending load and unstable boundary condition [6].

## II. OBJECTIVE

The objective is to design Rocker arms of HMCF UD and Carbon Steel EN6 using Solidworks 2013 and carry out the finite element analysis (FEA) on the prepared model using ANSYS 16. Thus, we obtained the values of various stresses and deformation. This result was then compared with the result from analysis with existing Structural Steel rocker arm.

## III. MATERIAL AND PROPERTIES

The general material used for rocker arms are Steel, Aluminum, Forged steel, Stainless steel, alloys and composites. Husain and Sheikh led to a conclusion that steel is better than aluminum in terms of strength while aluminum is better for low costing arms [4]. Sharief & Sushmitha analyzed a composite rocker arm of high density polyethylene (HDPE) reinforced with short S-glass fibers of 10% volume fraction [7].

HMCF UD and Carbon Steel EN 6 have been used for analysis. Carbon Steel EN 6 carbon steel is a medium strength steel. It is generally provided in square and flat round bar as key steel [8]. Composite like High Modulus Carbon Fibre Unidirectional (HMCF UD) are not common in practice but they are extremely lightweight with considerably good strength.

TABLE I: MATERIAL PROPERTIES

Material	Carbon Steel EN 6	HMCF UD	Structural Steel
Density (g/cm <sup>3</sup> )	7.85	1.6	7.85
Young's Modulus (GPa)	200	175	200
Ultimate Tensile Strength (MPa)	585	1000	460
Poisson's Ratio	.285	0.3	0.3

## IV. DESIGN AND CALCULATIONS

### A. Nomenclature:

- $m_v$  = mass of valve
- $w$  = weight of associated parts with valve
- $d_v$  = diameter of valve
- $h$  = lift of valve
- $a$  = Acceleration of the valve
- $P_c$  = Cylinder pressure
- $P_s$  = Maximum suction pressure
- $d_f$  = fulcrum pin diameter
- $d_b$  = diameter of boss
- $l$  = Length of arm
- $\theta$  = angle subtended by arms with respect to each other
- $P_g$  = Gas load on the valve
- $P_t$  = Total load on the valve
- $F_i$  = Initial Spring Force
- $F_a$  = Force due to acceleration of valve
- $P_e$  = Maximum load on the rocker arm for exhaust valve
- $t$  = Valve closing/ opening time
- $N$  = Rpm of the engine
- $N_c$  = Speed of camshaft
- $R_f$  = Reaction at fulcrum pin

**TABLE II: ENGINE SPECIFICATION**

Type	Turbo charged, Common rail injection Diesel Engine
No. Of Cylinders	6- V configuration
Bore/Stroke	84mm x 90mm
Capacity	2,933 cc
Max. Engine Output	182 Kw @ 4200 rpm
Max. Torque	600 N-m @

$$\begin{aligned}
 m_v &= 0.09 \text{ kg} \\
 d_v &= 40 \text{ mm} \\
 h &= 13 \text{ mm} \\
 r &= \frac{h}{2} = 6.5 \text{ mm} \\
 P_c &= 0.4 \text{ N/mm}^2 \\
 P_s &= 0.02 \text{ N/mm}^2 \\
 d_f &= 8 \text{ mm} \\
 d_b &= 18 \text{ mm} \\
 \theta &= 110^\circ
 \end{aligned}$$

### B. Force Calculation

1. Gas load on the valve:

$$\begin{aligned}
 P_g &= \frac{\pi}{4} \times d_v^2 \times P_c \\
 &= 502.4
 \end{aligned}$$

$$\begin{aligned}
 w &= m \times g \\
 &= 0.09 \times 9.8 \\
 &= 0.882 \text{ N}
 \end{aligned}$$

$$P_t = P_g + w = 503.282 \text{ N}$$

2. Spring Force

$$\begin{aligned}
 F_i &= \left( \frac{\pi}{4} \times d_v^2 \times P_s \right) - w \\
 &= 24.238 \text{ N}
 \end{aligned}$$

3. Force due to acceleration of valve

$$N_c = \frac{N}{2} = 2100 \text{ rpm}$$

4. Angle turned by camshaft per second,

$$\theta_c = \frac{2100}{60} \times 30 = 12600 \text{ deg/sec}$$

$$\begin{aligned}
 t &= \frac{\theta}{\theta_c} \\
 &= \frac{110}{12600} \\
 &= .009 \text{ sec} \\
 a &= \omega^2 \times r \\
 &= \left( \frac{2\pi}{t} \right)^2 \times r \\
 &= 3168.02 \text{ m/s}^2 \\
 F_a &= ma + w \\
 &= 286 \text{ N}
 \end{aligned}$$

5. Reaction at fulcrum pin

$$\begin{aligned}
 P_e &= P_t + F_i + F_a \\
 &= 503,282 + 24.238 + 286 \\
 &= 813.52
 \end{aligned}$$

Length of both the arms are equal,  
 $\Rightarrow P_c = P_e = 813.52$

$$\begin{aligned}
 R_f &= \sqrt{F_e^2 + F_i^2 - 2 \times F_e \times F_i \times \cos\theta} \\
 &= 1625.43 \text{ N}
 \end{aligned}$$

## V. METHODOLOGY

### A. Modelling in Solid works

The dimensions for the parts were determined analytically which were later used in modelling. The base of rocker body was an extruded entity. The extruded cut profiles were applied on the top. The model was saved in IGES format and imported to ANSYS workbench.

### B. Meshing

Figure shows the meshed model of rocker arm for analysis process. For analysis, model was meshed using triangular surface mesher. The number of Nodes used in this meshing is 31120 and elements are 17949. The model is meshed and analyzed to get the correct value. The high number of elements for chosen for better and authentic results.

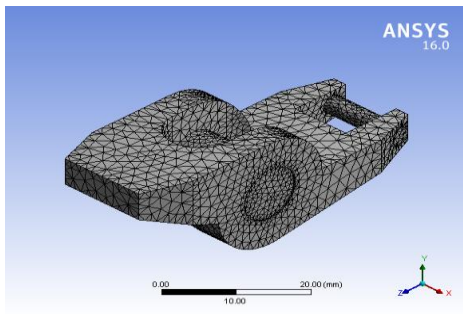


Fig. 3. Meshed Model

Fig. 6. Equivalent (Von- Mises) Strain for Structural steel rocker arm

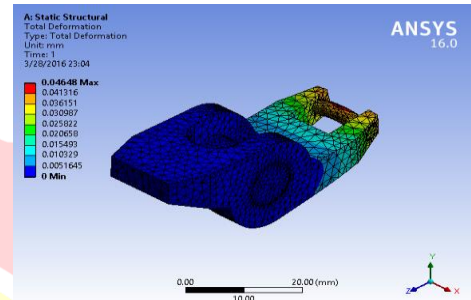


Fig. 7. Total deformation for HMCF UD rocker arm

## VI. ANALYSIS AND RESULTS

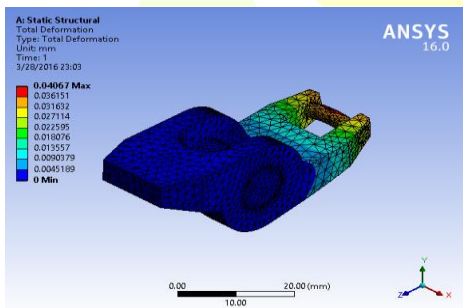


Fig. 4. Total deformation for structural steel rocker arm

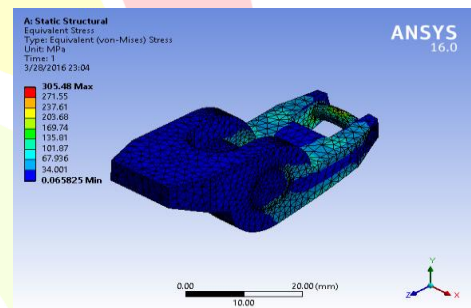


Fig. 8. Equivalent (Von- Mises) Stress for HMCF UD rocker arm

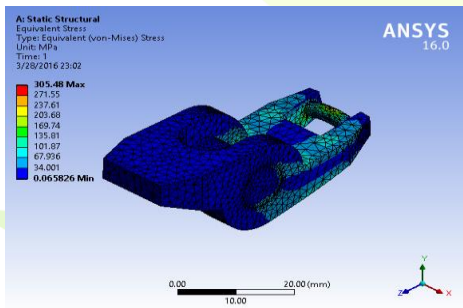


Fig. 5. Equivalent (Von- Mises) Stress for Structural steel rocker arm

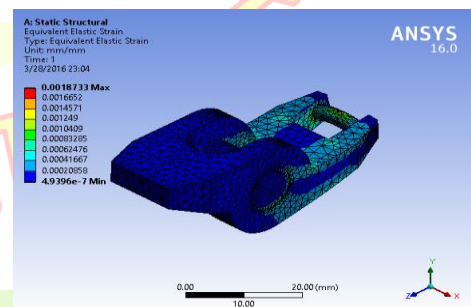


Fig. 9. Equivalent (Von- Mises) Strain for HMCF UD rocker arm

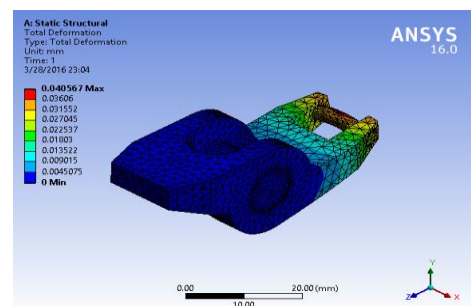
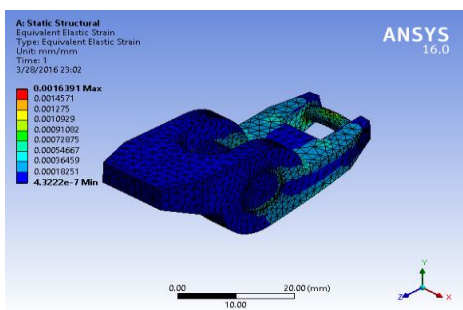




Fig. 10. Total deformation for Carbon Steel EN 6 rocker arm

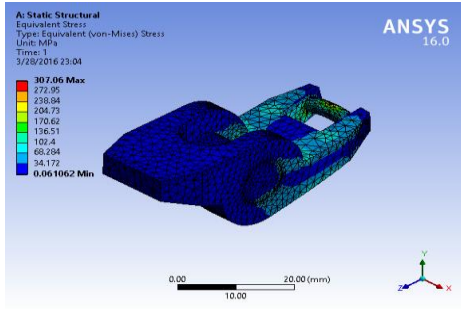


Fig. 11. Equivalent (Von- Mises) Stress for Carbon Steel EN 6 rocker arm

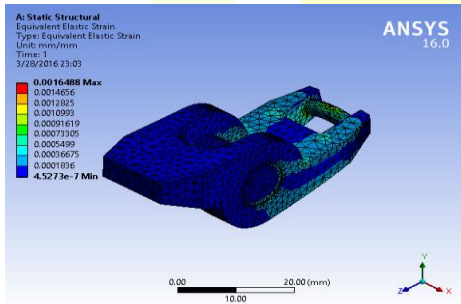


Fig. 12. Equivalent (Von- Mises) Strain for Carbon Steel EN 6 rocker arm

**TABLE III: RESULTS**

Material		Structural Steel	HMC F UD	Carb on Steel EN 6
Total Deformation (mm)	Max	0.0406	0.04648	0.040567
	Min	0	0	0
Equivalent Stress (MPA)	Max	305.48	305.48	307.06
	Min	0.0658	0.0658	0.061
Equivalent Elastic Strain (mm/mm)	Max	0.00169	0.00187	0.00164
	Min	4.322E-07	4.939E-07	4.527E-07

## VII. CONCLUSION

The Von-Mises stress values for Structural Steel, HMC F UD and Carbon Steel Carbon Steel EN 6 rocker arms are 305.48 MPa, 305.48 MPa and 307.06MPa. The total deformation for structural steel rocker arm is 0.04067 mm while the same for HMC F UD and Carbon Steel EN 6 rocker arm is 0.04648 mm and 0.040567 mm.

From the above results, it can be observed that a light weight and considerably high strength HMC F UD can be used as rocker arm. The composite rocker arm is able to withstand the load equivalent to that a structural rocker arm can. As for Carbon Steel EN 6, it is observed that for a lower deformation, it showed almost same value of stress, leading to the conclusion that it can be used for rocker arm. Hence, it can be concluded that both HMC F UD and Carbon Steel EN 6 can be used as material for rocker arm.

## VIII. REFERENCES

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